

**SOLUTIONS (TEST SERIES 2) PH**

1. (2) In the region where there exists a distribution of charge of volume charge density (i.e. charge per unit volume)  $\rho$ , the differential form of Gauss's law is

$$\text{div } \vec{E} = 4\pi\rho$$

[in CGS Gaussian system]

We have  $E = -\text{grad } V$

$$\therefore \text{div}(-\text{grad } V) = 4\pi\rho$$

$$-\vec{\nabla} \cdot \nabla V = 4\pi\rho$$

or  $\boxed{\nabla^2 V = -4\pi\rho}$

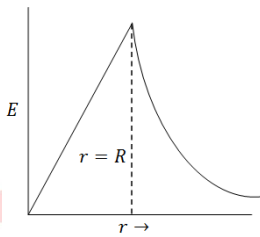
2. (3) The electric field strength due a non-conducting uniformly charged sphere of radius, when point lies outside the charge distribution i.e.,  $r > R$ , varies inversely with  $r$

i.e.,  $E \propto r^{-1}$

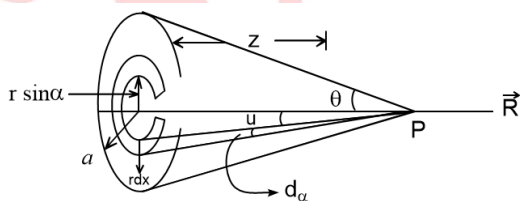
and when point lies inside the charge distribution i.e.,  $r < R$

$$E \propto r$$

Hence plot will be



3. (1) Magnetic scalar potential for a point on the Z-axis of a circular loop of radius  $a$



As  $d\Omega = \frac{ds}{r^2}$

For this case

$$\Omega = \int \frac{ds}{r^2} = \int_0^\theta \frac{(2\pi r \sin\alpha) r d\alpha}{r^2}$$

$$= 2\pi [-\cos\theta]_0^\theta$$

$$= 2\pi(1 - \cos\theta)$$

i.e.,  $\Omega = 2 \left[ 1 - \frac{z}{(a^2+z^2)^{1/2}} \right]$

as  $\cos\theta = \frac{z}{(a^2+z^2)^{1/2}}$

so magnetic scalar potential

$$\boxed{\begin{aligned} \Phi_m &= \frac{\mu_0 I}{4\pi} \Omega \\ &= \frac{\mu_0 I}{4\pi} 2\pi \left[ 1 - \frac{z}{(a^2+z^2)^{1/2}} \right] \end{aligned}}$$

4. (4)  $E_z = a \cos \omega x \cos \omega ct$

$$H_y = -a \sin \omega x \sin \omega ct$$

As  $\vec{S} = \vec{E} \times \vec{H}$

i.e.,  $S = a \cos \omega x \sin \omega x \cos \omega ct \sin \omega ct$

$$= -a^2 \cos \omega x \sin \omega x \cos \omega ct \sin \omega ct$$

$$= -a^2 \frac{\sin 2\omega x}{2} \cdot \frac{\sin 2\omega ct}{2}$$

$$\boxed{S = -\frac{1}{4} a^2 \sin 2\omega x \sin 2\omega ct}$$

5. (1) we have

$$\frac{dP}{d\Omega} = \frac{1}{4\pi\epsilon_0} \frac{e^2 a^2}{4\pi c^3} \sin^2 \theta$$

The total radiated power is obtained by integrating this equation

$$P = \int_{4\pi} \frac{dP}{d\Omega} d\Omega$$

$$= \int_{4\pi} \frac{1}{4\pi\epsilon_0} \frac{e^2 a^2}{4\pi c^3} \sin^2 \theta d\Omega$$

where,  $d\Omega = \frac{(R \sin \theta d\phi)(R d\theta)}{R^2}$

$$= \frac{1}{4\pi\epsilon_0} \frac{e^2 a^2}{4\pi c^3} \int_0^\pi \int_0^{2\pi} (\sin^2 \theta) \sin \theta d\theta d\phi$$

$$= \frac{1}{4\pi\epsilon_0} \frac{e^2 a^2}{4\pi c^3} \times 2\pi \int_0^\pi \sin^3 \theta d\theta$$

$$= \frac{1}{4\pi\epsilon_0} \frac{e^2 a^2}{4\pi c^3} \times 2\pi \times \frac{4}{3}$$

$$\boxed{P = \frac{1}{4\pi\epsilon_0} \frac{2 e^2 a^2}{3 c^3}}$$

- 6.

(1)  $W = - \int_{r_1}^{2r_1} Q \vec{E} \cdot d\vec{r}$

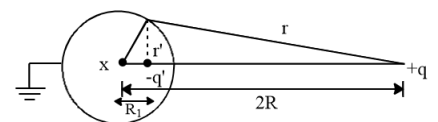
$$= - \int_{r_1}^{2r_1} Q \cdot \frac{k}{r} dr = - [Qk \ln r]_{r_1}^{2r_1}$$

$$= -Qk [\ln(2r_1) - \ln r_1]$$

$$= -Qk \ln 2$$

- 7.

(1) Applying boundary condition for grounded conducting sphere



$$\frac{q}{4\pi\epsilon_0 r} = - \frac{q'}{4\pi\epsilon_0 r'}$$

or  $\frac{q}{r} = - \frac{q'}{r'}$

$$\Rightarrow \frac{q}{R^2 + (2R)^2 - 4R^2 \cos \theta}$$

$$= \frac{-q'}{R^2 + R_1^2 - 2R_1R \cos \theta}$$

So condition requires that

$$R^2 = 2RR_1$$

or  $R_1 = \frac{R}{2}$

and  $q' = -q\sqrt{\frac{R/2}{2R}}$   
 $= -q\sqrt{\frac{1}{4}}$   
 $= -\frac{q}{2}$

8. (2)  $E = \frac{q}{4\pi \epsilon_0 r^2}$

Since  $q_1 \rightarrow Q, q_2 \rightarrow 2Q$

$$r_1 \rightarrow r, r_2 \rightarrow \frac{r}{2}$$

$$\therefore \frac{E_1}{E_2} = \frac{\frac{Q}{4\pi \epsilon_0 r^2}}{\frac{2Q}{4\pi \epsilon_0 \left(\frac{r}{2}\right)^2}} = \frac{Q}{r^2} \times \frac{\left(\frac{r}{2}\right)^2}{2Q}$$

$$\frac{E_1}{E_2} = \frac{1}{8}$$

or  $E_2 = 8E_1$

9. (1)  $V = -E_0 \left(1 - \frac{R^3}{r^3}\right) r \cos \theta$

The charge density is related to  $\bar{E}$  by relation

$$\bar{E} = \frac{\sigma}{\epsilon_0}$$

or  $\sigma = \epsilon_0 \bar{E}$

since  $\bar{E} = -\nabla V$

$$\sigma = -\epsilon_0 \left. \frac{\partial V}{\partial r} \right|_{at r=R}$$

$$= -\epsilon_0 \left[ -E_0 \cos \theta - \frac{2R^3}{r^3} \cos \theta E_0 \right]_{r=R}$$

$$= -\epsilon_0 [-E_0 \cos \theta - 2E_0 \cos \theta]$$

$$\sigma = 3\epsilon_0 E_0 \cos \theta$$

10. (1)

11. (3) The work done in bringing the charge from  $x = \infty$  to  $d$  is

$$W = \int_{x=\infty}^d \vec{F} \cdot d\vec{r}$$

$$= - \int_{x=\infty}^d \left( -\frac{q^2}{4\pi \epsilon_0 (2x)^2} \hat{i} \right)$$

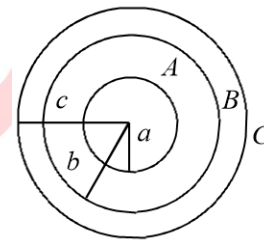
$$= + \frac{q^2}{16\pi \epsilon_0} \int_{x=\infty}^d \frac{1}{x^2} dx$$

$$= -\frac{q^2}{16\pi \epsilon_0 d}$$

$$= -\frac{q^2}{4\pi \epsilon_0 (4d)}$$

12. (3) Potential at C

$V_c =$  pot. due to  $\sigma$  on A + pot. due to  $-\sigma$  on B + pot. due to  $\sigma$  on C



$$= \frac{1}{4\pi \epsilon_0} \left( \frac{4\pi a^2 \sigma}{c} \right) + \frac{1}{4\pi \epsilon_0} \left( \frac{-4\pi b^2 \sigma}{c} \right)$$

$$+ \frac{1}{4\pi \epsilon_0} \left( \frac{4\pi c^2 \sigma}{c} \right)$$

$$= \frac{\sigma}{\epsilon_0} \left( \frac{a^2}{c} - \frac{b^2}{c} + c \right)$$

13. (2) using Laplace equation

$$\frac{\partial}{\partial r} \left( r^2 \frac{\partial V}{\partial r} \right) = 0$$

$$\Rightarrow r^2 \frac{dV}{dr} = A$$

i.e.  $V = -\frac{A}{r} + B$  .....(i)

but  $V = V_a$  at  $r = a$

i.e.  $V_a = -\frac{A}{a} + B$

and  $V = V_b$  at  $r = b$

i.e.  $V_b = -\frac{A}{b} + B$  .....(iii)

eliminating A and B from equation (ii) and (iii) and substitute in equation (i), we get

$$V = \frac{ab(V_a - V_b)}{b-a} \cdot \frac{1}{r} + \frac{bV_b - aV_a}{b-a}$$

Now  $V_a$  is at  $V_0$  and  $V_b = 0$  (according to problem)

$$\therefore V = \frac{abV_0}{b-a} \cdot \frac{1}{r} - \frac{aV_0}{b-a}$$

$$\text{or } V = \frac{aV_0}{b-a} \left[ \frac{b}{r} - 1 \right]$$

$$14. (2) \quad \vec{\sigma} = \vec{p} \cdot \hat{n} = P_0 \hat{k} \cdot \hat{n}$$

$$\therefore \boxed{\sigma = p_0}$$

and volume charge density

$$\begin{aligned} \rho &= -\vec{\nabla} \cdot \vec{P} \\ &= -\vec{\nabla} \cdot (p_0 \hat{k}) \end{aligned}$$

$$\therefore \boxed{\rho = 0}$$

$$15. (2) \text{ Magnetic moment} = nIA$$

$$M = nI\pi R^2$$

Now  $I \rightarrow I/2$  and  $R \rightarrow 2R$

$$\begin{aligned} M_2 &= n \cdot \frac{I}{2} \pi (2R)^2 \\ &= 2nI\pi R^2 = 2M \end{aligned}$$

$$16. (1)$$

$$17. (1) \text{ we know}$$

$$\oint \vec{B} \cdot d\vec{l} = \mu_0 I$$

$$I = \frac{dq}{dt}$$

Since

$$= \frac{d}{dt} (\sigma A) = \sigma \frac{dA}{dt}$$

$$\therefore B \cdot 2\pi R = \mu_0 \sigma \frac{ds}{dt}$$

$$\Rightarrow B = \frac{\mu_0 \sigma}{2\pi R} \frac{ds}{dt}$$

Now surface current

$$J_s = M = \frac{B}{\mu_0} = \frac{\sigma}{2\pi R} \cdot \frac{ds}{dt}$$

$$\text{Area (s)} = \pi R^2$$

$$\frac{ds}{dt} = 2\pi R \frac{dR}{dt} = 2\pi R \omega R$$

$\therefore$  surface current

$$J_s = \frac{\sigma}{2\pi R} \times 2\pi R^2 \cdot \omega$$

$$\boxed{J = \sigma R \omega}$$

$$18. (3)$$

$$19. (3) \text{ force for moving charge}$$

$$\vec{F} = q\vec{v} \times \vec{B}$$

$$BE_1 = KE_2$$

$$\therefore 1:1$$

$$20. (1) \text{ Elliptically since}$$

$$F_x \neq F_y$$

$$21. (3)$$

$$22. (1)$$

$$23. (3) \text{ we know}$$

$$\frac{E_{0r}}{E_{0i}} = \frac{n_2 - n_1}{n_2 + n_1}$$

$$\frac{E_{0t}}{E_{0i}} = \frac{2n_1}{n_2 + n_1}$$

$$\Rightarrow E_{0r} = E_{0i} \left[ \frac{1 - \frac{n_2}{n_1}}{\frac{n_2}{n_1} + 1} \right]$$

$$= 2 \times \frac{1.5 - 1}{1.5 + 1} = -2 \times \frac{0.5}{2.5}$$

$$= -\frac{2}{5} \text{ V/m}$$

$$\text{and for } E_{0t} = E_{0i} \times \frac{2}{1 + \frac{n_2}{n_1}}$$

$$= 2 \times 2 \times \frac{1}{5} \times 2$$

$$\boxed{E_{0t} = \frac{8}{5} \text{ V/m}}$$

$$24. (4)$$

$$25. (2)$$

$$26. (4)$$

$$27. (1)$$

$$28. (2) \quad m = 2, n = 1, \beta_p = 12, f = 6\text{GHz}$$

$$\beta_p = \frac{\omega}{v} \sqrt{1 - \left( \frac{f_c}{f} \right)^2}$$

$$12 = \frac{2\pi \times 6 \times 10^9}{3 \times 10^8} \sqrt{1 - \left(\frac{f_c}{6}\right)^2}$$

$$f_c = 5.973 \text{GHz}$$

$$29. (1) f_r = \frac{v}{2} \sqrt{\left(\frac{m}{a}\right)^2 + \left(\frac{n}{b}\right)^2 + \left(\frac{p}{c}\right)^2}$$

where for TM mode to Z

$$m = 1, 2, 3, \dots, n = 1, 2, 3, \dots, p = 0, 1, 2, \dots$$

For TE mode to Z

$$m = 1, 2, 3, \dots; n = 1, 2, 3, \dots; p = 1, 2, 3, \dots$$

If  $a < b < c$ , then  $\frac{1}{a} > \frac{1}{b} > \frac{1}{c}$

The lowest TM mode is  $TM_{110}$ , with

$$f_{r_1} = \frac{v}{2} \sqrt{\left(\frac{1}{a}\right)^2 + \left(\frac{1}{b}\right)^2}$$

The lowest TE mode is  $TE_{011}$ , with

$$f_{r_2} = \frac{v}{2} \sqrt{\left(\frac{1}{b}\right)^2 + \left(\frac{1}{c}\right)^2}$$

$$f_{r_1} > f_{r_2}$$

$$30. (2) f_c = \frac{C}{2\sqrt{\epsilon_r}} \sqrt{\left(\frac{m}{a}\right)^2 + \left(\frac{n}{b}\right)^2}$$

$$f_{c10} = \frac{C}{2a\sqrt{\epsilon_r}} = \frac{2 \times 10^8}{2 \times 1.25 \times 0.06}$$

$$= 2 \text{GHz}$$

$$31. (1) f < f_c$$

$$f < \frac{v}{2b} = \frac{3 \times 10^8}{2 \times b \times \sqrt{2.1}}$$

$$3 \times 10^9 < \frac{3 \times 10^8}{2 \times b \times \sqrt{2.1}}$$

$$b < 3.4 \text{cm}$$

$$32. \langle v_x^2 v_y^2 v_z^2 \rangle =$$

$$N \left(\frac{m}{2\pi K T}\right)^{\frac{3}{2}} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} v_x^2 v_y^2 v_z^2 e^{-\frac{m(v_x^2 v_y^2 v_z^2)}{2K_B T}} dv_x dv_y dv_z$$

$$\frac{m v_x^2}{2KT} = x$$

$$v_x = \sqrt{\frac{2KT}{m}} \cdot x^{1/2}$$

$$\int_{-\infty}^{\infty} v_x^2 e^{-\frac{m v_x^2}{2KT}} dv_x = \frac{2KT}{m} \int_{-\infty}^{\infty} x e^{-x} \cdot \sqrt{\frac{2KT}{m}} \frac{1}{2} x^{-1/2} dx$$

$$= \frac{2KT}{m} \sqrt{\frac{2KT}{m}} \cdot \int_0^{\infty} x^{\frac{1}{2}} e^{-x} dx$$

$$= \left(\frac{2KT}{m}\right)^{3/2} \cdot \left[\frac{3}{2}\right]$$

$$= \left(\frac{2KT}{m}\right)^{3/2} \cdot \frac{1}{2} \sqrt{\pi}$$

$$\therefore \langle v_x^2 v_y^2 v_z^2 \rangle = N \left(\frac{m}{2\pi K T}\right)^3 \cdot \left(\frac{2KT}{m}\right)^{\frac{9}{2}} \cdot \frac{1}{8} \pi^{\frac{3}{2}}$$

$$= N \left(\frac{m}{2\pi K}\right) \cdot \left(\frac{2K}{m}\right) \cdot \frac{1}{8} \pi^{3/2} \cdot T^3$$

$$\boxed{\langle v_x^2 v_y^2 v_z^2 \rangle = \alpha T^3}$$

$$\therefore \langle v_x^2 v_y^2 v_z^2 \rangle \alpha T^3$$

$$33. \lambda_m T = \text{Constant}$$

$$\therefore \frac{T_S}{T_P} = \frac{\lambda_P}{\lambda_S} = \frac{380}{500}$$

$$\boxed{\frac{T_S}{T_P} = 0.76}$$

34. Let heat extracted from object be  $dQ$  and temperature be  $T$ .

Efficiency of heat engine

$$\eta = \left(1 - \frac{T_2}{T}\right) \text{ (assuming maximum efficiency)}$$

Work  $dW = \eta dQ$

$$= \left(1 - \frac{T_2}{T}\right) dQ$$

$$= \left(1 - \frac{T_2}{T}\right) C_p dT$$

$\therefore$  Total work done at  $T_2$

$$\omega = \int \left(1 - \frac{T_2}{T}\right) C_p dT$$

$$= C_p [T - T_2 \ln T]_{T_1}^{T_2}$$

$$\boxed{\omega = C_p (T_2 - T_1) - C_p T_2 \ln T_2 / T_1}$$

35. According to statistical entropy, we have

$$S = K_B \ln \Omega \quad \dots (1)$$

Now number of microstates for N-identical Spin zero particles is

$$\Omega_1 = (2S + 1)^N = (2 \times 0 + 1)^N = 1^N \dots (2)$$

And for 2N identical spin half particles

$\therefore$  Number of microstates for N-identical spin  $\frac{1}{2}$  is

$$\Omega_2 = (2S + 1)^N$$

$$= \left(2 \times \frac{1}{2} + 1\right)^N$$

$$\Omega_2 = 2^N$$

So, total number of microstates

$$\Omega = \Omega_1 \Omega_2$$

$$S = K_B \ln(1^N \cdot 2^N)$$

$$= NK_B \ln 2$$

$$= 1000 K_B \ln 2$$

$$= 1000 K_B \times 0.6931$$

$$S = 693.1 K_B$$

$$36. \quad \gamma = \frac{C_P}{C_V} = 1.4$$

For adiabatic process

$$TP^{1-\gamma/\gamma} = \text{Constant}$$

$$T_i P_i^{1-\gamma} = T_f P_f^{1-\gamma}$$

$$T_f = \left(\frac{P_i}{P_f}\right)^{\frac{1-\gamma}{\gamma}} T_i$$

$$= T_i 2^{-2/7}$$

$$= \frac{288}{2^{2/7}} = 236.3 K = -36.7^\circ C$$

37. (1)

$$38. \quad P = P_0 e^{-\alpha V}$$

$$T = \frac{PV}{nR} = \frac{P_0 e^{-\alpha V}}{nR} \cdot V$$

To maximise T, take derivative and make it equal to zero

$$\frac{dT}{dV} = \frac{P_0}{nR} [e^{-\alpha V} - \alpha V e^{-\alpha V}] = 0$$

$$\therefore V = 1/\alpha$$

$$\text{Given } T = \frac{P_0 e^{-\alpha V}}{nR}$$

$$\text{For } T_{\max} = \frac{P_0 e^{-\alpha \cdot \frac{1}{\alpha}}}{nR} \cdot \frac{1}{\alpha}$$

$$= \frac{P_0 e^{-1}}{\alpha nR}$$

$$T_{\max} = \frac{P_0}{e \alpha nR}$$

39. (3)

40. (1) According to Wien's displacement law

$$\lambda_m T = \text{Constant}$$

$$\Rightarrow \lambda_m \propto \frac{1}{T}$$

$$\text{or, } v_{\max} \propto T$$

So, if  $v_{\max}$  becomes half, T will also become half.

$$T_2 = \frac{T_1}{2}$$

41. (2)

$$\frac{dQ}{dt} = \frac{KA\Delta T}{L}$$

$$\log\left(\frac{dQ}{dt}\right) = \log K + \log A + \log \Delta T - \log L$$

$$\frac{\Delta \frac{dQ}{dt}}{\frac{dQ}{dt}} = \frac{\Delta K}{K} + \frac{\Delta A}{A} + \frac{\Delta(\Delta T)}{\Delta T} + \frac{\Delta L}{L}$$

$$\frac{\Delta K}{K} = \frac{\Delta \frac{dQ}{dt}}{\frac{dQ}{dt}} - \frac{\Delta A}{A} - \frac{\Delta(\Delta T)}{\Delta T} - \frac{\Delta L}{L}$$

absolute erosion

$$\left|\frac{\Delta K}{K}\right| = \left|\frac{\Delta \frac{dQ}{dt}}{\frac{dQ}{dt}}\right| + \left|\frac{\Delta A}{A}\right| + \left|\frac{\Delta(\Delta T)}{\Delta T}\right| + \left|\frac{\Delta L}{L}\right|$$

Assuming error in cross-section area to be zero maximum proportional error in measurement of thermal conductivity = 90%

42. (3) Let  $\eta_1$  and  $\eta_2$  be the efficiencies of both the heat engines

$$W_1 = \eta_1 Q_1 = \left(1 - \frac{T_2}{T_1}\right) Q_1$$

$$W_2 = \eta_2 Q_2 = \left(1 - \frac{T_3}{T_2}\right) Q_2$$

$$= \left(1 - \frac{T_3}{T_2}\right) \frac{T_2}{T_1} Q_1$$

Total work done

$$\begin{aligned}
W &= W_1 + W_2 & 48. (4) \\
&= \left(1 - \frac{T_2}{T_1}\right) Q_1 + \left(1 - \frac{T_3}{T_2}\right) \frac{T_2}{T_1} Q_1 & 49. (3) \\
&= \left[1 - \frac{T_2}{T_1} + \frac{T_2}{T_1} - \frac{T_3}{T_1}\right] Q_1 & 50. (3) \\
&= \left(1 - \frac{T_3}{T_1}\right) Q_1 & 51. (2) \\
& & 52. (3) \\
& & 53. (3) \\
& & 54. (1) \\
& & 55. (4) \\
& & 56. (4) \\
& & 57. (1) \\
& & 58. (2) \\
& & 59. (1) \\
& & 60. (4)
\end{aligned}$$

$$\text{Net efficiency } \eta = \frac{W}{Q_1} = \left(1 - \frac{T_3}{T_1}\right)$$

43. (1) RMS velocities of the molecules are

$$\begin{aligned}
V_1 &= \sqrt{\frac{8kT}{\pi m}} \\
V_2 &= \sqrt{\frac{8kT}{4\pi m}} = \frac{1}{2} \sqrt{\frac{8kT}{\pi m}}
\end{aligned}$$

Root mean square velocity of atoms in the mixture

$$V = \frac{V_1 + V_2}{2} = \frac{3}{4} \sqrt{\frac{8kT}{\pi m}}$$

Since the number of molecules are equal

44. (4)

45. (4)

46. (1)

47.  $H = -\mu B \sum_i S_i$

$$Z = \sum e^{-\beta H} = \sum e^{+\beta \mu B} \sum S_i$$

$$Z = e^{\mu B \beta} + e^{-\mu B \beta}$$

$$\langle S_i \rangle = \sum S_i P$$

$$= \sum S_i \frac{e^{+\mu B \beta} \sum S_i}{Z}$$

$$\langle S_i \rangle = \frac{e^{\mu B \beta} - e^{-\mu B \beta}}{e^{\mu B \beta} + e^{-\mu B \beta}}$$

$$\frac{1}{3} \geq \frac{e^{\mu B \beta} - e^{-\mu B \beta}}{e^{\mu B \beta} + e^{-\mu B \beta}}$$

$$e^{\mu B \beta} + e^{-\mu B \beta} \geq 3e^{\mu B \beta} - 3e^{-\mu B \beta}$$

$$4e^{-\mu B \beta} \geq 2e^{\mu B \beta}$$

$$2 \geq e^{2\mu B \beta}$$

$$\ln 2 \geq 2 \frac{\mu B}{K_B T} \Rightarrow \frac{1}{2} \ln 2 \geq \frac{\mu B}{K_B T}$$